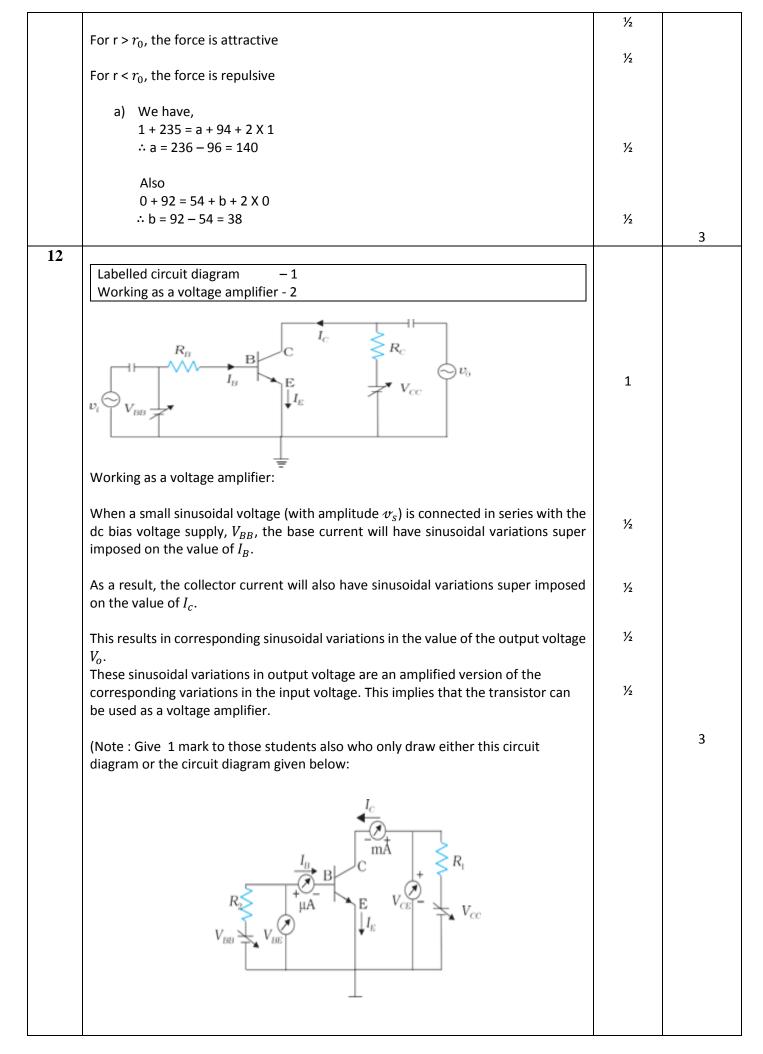
## MARKING SCHEME( COMPARTMENT) 2018

## SET 55/2

| Q.NO. | VALUE POINTS/ EXPECTED ANSWERS  | MARKS | TOTAL<br>MARKS |
|-------|---|-------|----------------|
|       | SECTION A   |       |                |
| 1     | relative<br>intensity   | 1     |                |
|       | position on screen  |       | 1              |
| 2     | Normal : Circular   | 1/2   |                |
|       | At an angle of $30^0$ it will follow helical path   | 1∕2   | 1              |
| 3     | The power of a lens equals to the reciprocal of its focal length( in meter).<br>Also accept                     | 1/2   |                |
|       | $p = \frac{1}{f(meter)}$<br>Do not deduct mark if student does not write the word meter.                        | 1/2   |                |
|       | (Alternatively<br>Power of a lens is the ability of conversion /diversion of the rays incident on<br>the lens.) |       |                |
|       | SI Unit: Dioptre(D)   |       | 1              |
| 4     | From few MHz to 30-40 MHz   |       | 1              |
| 5     | $v = \sqrt{\frac{2eV}{m}}$  | 1     | 1              |
|       | SECTION B   |       |                |
| 6     | Formula <sup>1</sup> /2   |       |                |
|       | (i) Frequency of first case <sup>1</sup> / <sub>2</sub>   |       |                |
|       | (ii) Frequency of second case 1/2<br>Ratio 1/2  |       |                |
|       |   |       |                |
|       |   |       |                |
|       |   |       |                |
|       |   |       |                |

|   | We have   |     |   |
|---|---|-----|---|
|   | $h\nu = E_f - E_i$  |     |   |
|   | $E_{0}$ $E_{0}$   |     |   |
|   | $=\frac{E_0}{n_f^2} - \frac{E_0}{n_i^2}$  | 1/  |   |
|   |   | 1/2 |   |
|   | ( <i>i</i> ) $hv_1 = E_0(\frac{1}{1^2} - \frac{1}{2^2}) = E_0 \times \frac{3}{4}$ |     |   |
|   | $(1) hv_1 = E_0(\frac{1}{1^2} - \frac{1}{2^2}) = E_0 \times \frac{1}{4}$          | 1/  |   |
|   |   | 1/2 |   |
|   | $(ii) hv_2 = E_0(\frac{1}{2^2} - \frac{1}{\infty^2}) = E_0 \times \frac{1}{4}$    |     |   |
|   | $2^{2} \propto 2^{2} \propto 2^{2} \propto 4$                                     | 1/2 |   |
|   | $v_{1} - 2$   |     |   |
|   | $\therefore \frac{v_1}{v_2} = 3$  |     |   |
|   | · 2   | 1/2 | 2 |
|   |   |     |   |
| 7 |   |     |   |
|   | (a)Definition <sup>1</sup> / <sub>2</sub>   |     |   |
|   | Relation <sup>1</sup> / <sub>2</sub>  |     |   |
|   | (b) Identification of A and B $\frac{1}{2} + \frac{1}{2}$                         |     |   |
|   |   |     |   |
|   |   |     |   |
|   | (a) Measure of the response of magnetic material to an external magnetic field.   |     |   |
|   | Also accept   | 1/2 |   |
|   |   |     |   |
|   | $\chi = \frac{ M }{ H }$  |     |   |
|   | $\chi^{-} H $   |     |   |
|   | We have   |     |   |
|   |   |     |   |
|   | $\chi = (\mu_r - 1)$  | 1/2 |   |
|   | (b) 0.96 : Diamagnetic  | 1/  |   |
|   | 500 : Ferromagnetic   | 1/2 |   |
|   |   | 1/2 | 2 |
| 8 |   |     |   |
| Ũ | SHM nature of oscillation of the wire AB <sup>1</sup> / <sub>2</sub>              |     |   |
|   | Expression for instantaneous magnetic flux <sup>1</sup> / <sub>2</sub>            |     |   |
|   |   |     |   |
|   | 1   |     |   |
|   | Qualitative explanation1/2  |     |   |
|   |   |     |   |
|   | The wire AB would oscillate in a simple harmonic way                              |     |   |
|   | We can write  | 1/2 |   |
|   | $x = -a\cos\omega t$  | /2  |   |
|   | (as x = -a at t = 0)  |     |   |
|   | Therefore Instantaneous magnetic Flux   |     |   |
|   | $\phi(t) = Blx$ $(l = AB)$  | 1/  |   |
|   | $\varphi(t) = Bix$ $(t = HB)$<br>Instantaneous induced emf                        | 1/2 |   |
|   |   |     |   |
|   | 14  |     |   |
|   | $e(t) = -\frac{d\phi}{dt} = aBl\omega \sin \omega t$                              | 1/2 |   |
|   |   |     |   |
|   | The induced emf, therefore varies with time sinusoidally.                         | 1/2 |   |
|   |   |     |   |
|   | ( Alternatively   |     |   |
|   | Arm AB executes SHM under the influence of restoring force developed in           |     |   |
|   | the spring, consequently an induced emfis produced across the ends of             |     |   |
|   | moving armAB which varies sinusoidally.)  |     |   |
|   | 6   |     |   |
|   |   |     | 2 |

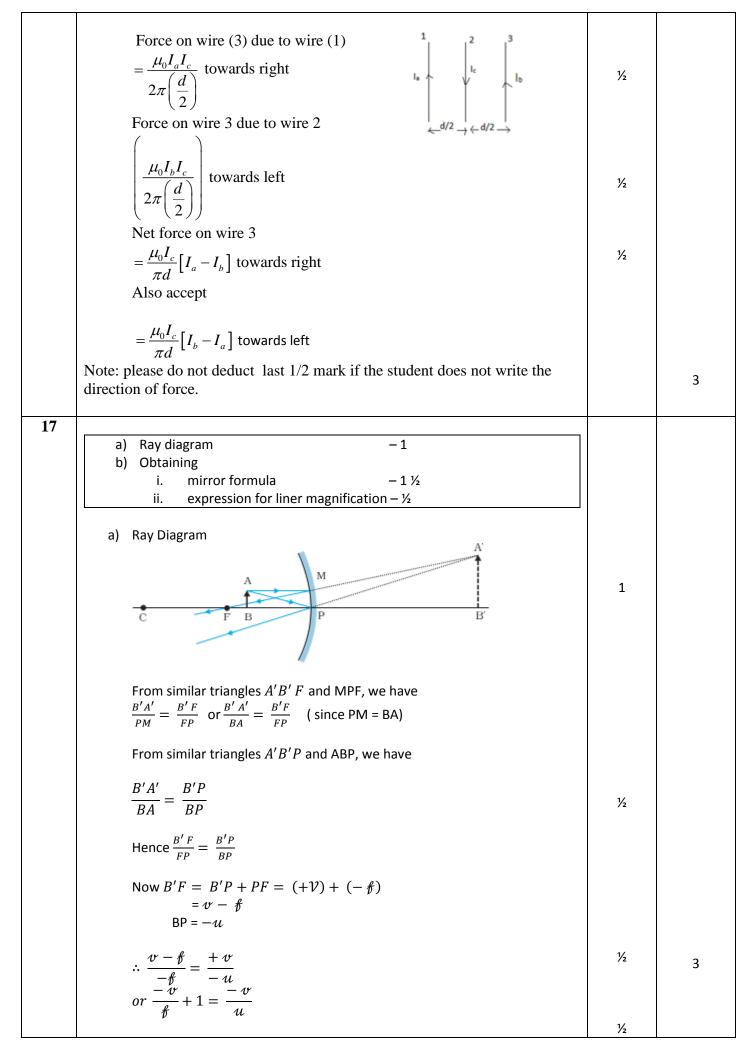
| 9  |  |     |   |
|----|--|-----|---|
| 9  | Formula1/2(iii)Frequency of first case1/2(iv)Frequency of second case1/2Ratio1/2   |     |   |
|    | We have  |     |   |
|    | $h\nu = E_f - E_i$ $= \frac{E_0}{n_f^2} - \frac{E_0}{n_i^2}$   | 1/2 |   |
|    | $(i)hv_1 = E_0(\frac{1}{1^2} - \frac{1}{2^2}) = E_0 \times \frac{3}{4}$  | 1/2 |   |
|    | $(ii) hv_2 = E_0(\frac{1}{2^2} - \frac{1}{\infty^2}) = E_0 \times \frac{1}{4}$   | 1/2 |   |
|    | $\therefore \frac{v_1}{v_2} = 3$   | 1/2 | 2 |
| 10 | (a) One use $1$<br>(b) One example each $\frac{1}{\frac{1}{2}+\frac{1}{2}}$  |     |   |
|    | (a) used to destroy cancer cells   | 1   |   |
|    | (b) (i)The region, between the plates of a capacitor, connected to time varying voltage source,has a displacement current but no conduction current.               | 1∕₂ |   |
|    | (ii) The wires, connected to the plates of a capacitor, joined to a time varying or steady voltage source, carry a conduction current but no displacement current. | 1∕₂ |   |
|    | (Alternatively<br>A circuit, having no capacitor in it, and carrying a current has conduction<br>current but no displacement current.)                             |     | 2 |
| 11 | SECTION C  |     |   |
| 11 | <ul> <li>a) Drawing the plot -1<br/>Marking the relevant regions - ½ + ½</li> <li>b) Finding values of a and b - ½+ ½</li> </ul>                                   |     |   |
|    | a) $bit = 1$   | 1   |   |



13  
(a) Statement of Biot-Savart law ½ Mark  
Its vector form ½ Mark  
(b) Obtaining the required expression 2 Mark  
(c) Obtaining the square of the distance r.  
Its direction is perpendicular to the plane containing dĪ and 
$$\bar{r}$$
.  
(c) Obtaining dĪ and  $\bar{r}$ .  
(c) Obtaining dI and  $\bar{r}$ .  
(c) Obta

| Definition of Electric flux1SI unit1/2Formula (Gauss's Law)1/2Calculation of Charge within the cube1   |          |   |
|--|----------|---|
| SI unit½Formula (Gauss's Law)½   |          |   |
| Formula (Gauss's Law) <sup>1</sup> / <sub>2</sub>  |          |   |
|  |          |   |
| Calculation of Charge within the cube 1  |          |   |
|  |          |   |
| Electric Elun is the det module of electric field and once meter   |          |   |
| Electric Flux is the dot product of electric field and area vector.  | 1        |   |
| Also Accept  |          |   |
| $\varphi = \oint \vec{E} \cdot \vec{ds}$   | 14       |   |
| SI Unit : $Nm^2/C$ or volt -meter  | 1/2      |   |
| For a given case   |          |   |
| $\phi = \phi_1 + \phi_2 = \left[ E_x(at \ x = 2a) - E_x(at \ x = a) \right] a^2$   |          |   |
|  |          |   |
| $= \left[ \alpha(2a) - \alpha(a) \right] a^2$  |          |   |
| $= \alpha a^3$   |          |   |
|  |          |   |
| $=100 \times (0.1)^3 = 0.1 Nm^2 / C$   | 1/2      |   |
| But  |          |   |
| d q  |          |   |
| $\phi = \frac{q}{\varepsilon_0}$   | 1/2      |   |
|  |          |   |
| $\therefore q = \varepsilon_0 \phi = 8.854 \times 10^{-12} \times 10^{-1} C$   | 1/       |   |
| = 0.8854  pC   | 1/2      |   |
|  |          |   |
| OR   |          |   |
| Relevant formulae1   |          |   |
| Calculation of time taken by the electron 1  |          |   |
| Calculation of time taken by the proton 1  |          |   |
|  |          |   |
|  |          |   |
| We have  |          |   |
| Force =qE  |          |   |
| Acceleration a = $\frac{qE}{m}$  | 1/2      |   |
|  |          |   |
| Also   |          |   |
| $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$  |          |   |
| $s = \frac{1}{2}at^2  as u = 0$  |          |   |
| $\therefore t = \sqrt{\frac{2s}{a}}$   |          |   |
| $\therefore t = \sqrt{\frac{23}{2}}$   | 1/2      |   |
| v a  |          |   |
| (i) For the electron   | 1/       |   |
|  | 1/2      |   |
| $a = \frac{eE}{2}$   |          |   |
| $a = \frac{eE}{m}$   |          |   |
| m  |          |   |
| m  |          |   |
|  | 1/_      |   |
| m  | 1/2      |   |
| m<br>$\therefore t = \sqrt{\frac{3 \times 10^{-2} \times 9.1 \times 10^{-31}}{1.6 \times 10^{-19} \times 2.0 \times 10^4}}$<br>= 2.92 ns   | 1/2      |   |
| (ii) for proton  | 1/2      |   |
| (ii) for proton  |          |   |
| (ii) for proton  | ½<br>1∕2 |   |
| $m$ $\therefore t = \sqrt{\frac{3 \times 10^{-2} \times 9.1 \times 10^{-31}}{1.6 \times 10^{-19} \times 2.0 \times 10^4}}$ $= 2.92 ns$ (ii) for proton $t = \sqrt{\frac{2 \times 1.5 \times 10^{-2} \times 1.67 \times 10^{-27}}{1.6 \times 10^{-19} \times 2 \times 10^4}}$ | 1/2      | 3 |
| (ii) for proton  |          | 3 |

| 15 |  |                |   |
|----|--|----------------|---|
|    | Writing the two loop equations $\frac{1}{2} + \frac{1}{2}$ MarkFinding the current through DB $\frac{1}{2}$ MarksFinding the p.d. between B and D $\frac{1}{2}$ Mark   |                |   |
|    | Using Kirchoff's voltage rule, we have :<br>For loop DABD<br>$I_1 \times 1 + (1) + (-2) + 2I_1 + 2(I_1 + I_2) = 0$<br>Or $5I_1 + 2I_2 = 1$ (i)   | ¥2             |   |
|    | For loop DCBD<br>+ $l_2 \times 3 + (3) + (-1) + l_2 + 2(l_1 + l_2) = 0$<br>Or $2l_1 + 6 l_2 = -2$ (ii)<br>Solving (i) and (ii), we get   | 1/2            |   |
|    | $I_1 = \frac{5}{13} A$   | 1/2            |   |
|    | $I_2 = \frac{-6}{13} A$  | 1/2            |   |
|    | $\therefore \text{ Current through DB} = I_1 + I_2 = \frac{-1}{13} \text{ A}$  | 1/2            | 3 |
|    | $\therefore$ P.D. between B and D = 0.154 V  | γ <sub>2</sub> |   |
|    |  |                |   |
| 16 | <ul> <li>(a) Definition of SI unit Of current <ol> <li>Explanation of the force of attraction</li> <li>Explanation of the force of attraction</li> <li>Finding the resultant force acting on the third conductor</li> </ol> </li> <li>(a) The <i>ampere</i> is the value of that steady current which, when maintained in each of the two very long, straight, parallel conductors of negligible cross-section, and placed one metre apart in vacuum, would produce on each of these conductors a force equal to 2 × 10<sup>-7</sup> newton per metre of length.</li> <li>(b) The wire (b) experiences a force due to the magnetic field caused by the current flowing in wire (a).</li> </ul> | 1              |   |
|    | The magnetic field at any point on the wire (b) due to the current in wire (a) is is perpendicular to the plane of two wires and pointing inwards and hence force on it will be towards wire (a). Similarly force on wire (a) will be towards wire (b). Hence two wires carrying currents in same direction attract each other.  | 1/2            |   |



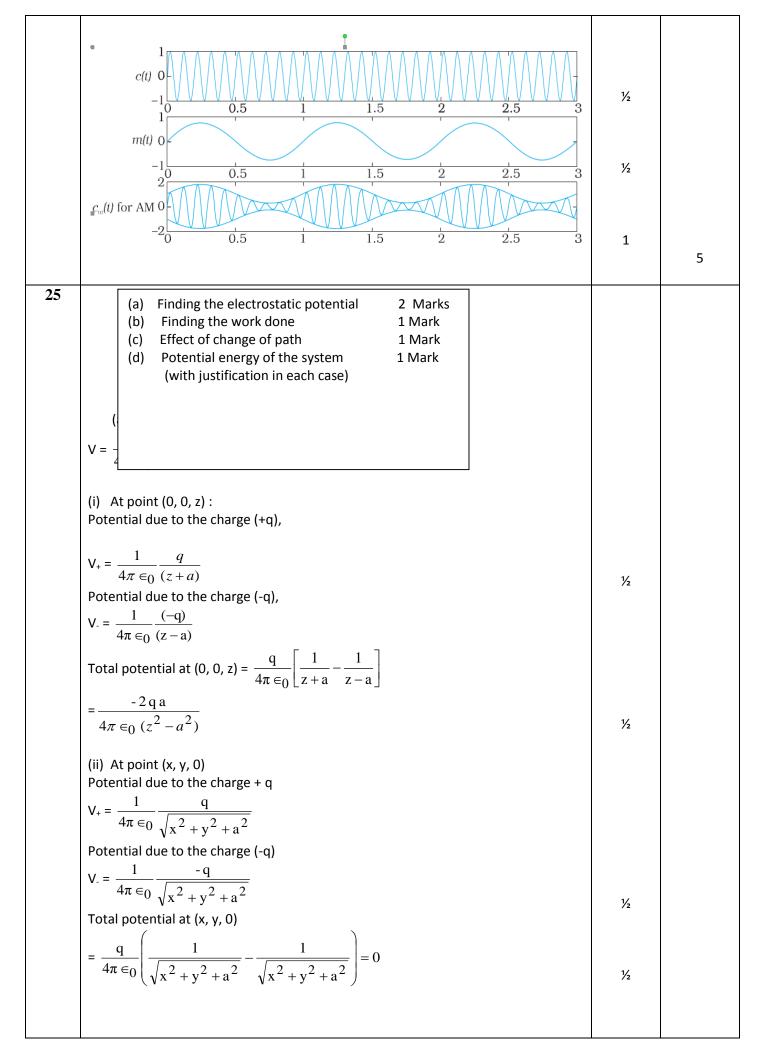
| $\therefore \frac{1}{v} + \frac{1}{u} = \frac{1}{t}$   |                |   |
|--|----------------|---|
| This is the mirror formula.  |                |   |
| Linear magnification = $\frac{B'A'}{BA}$   |                |   |
| From similar triangles $A'B'P$ and ABP, we get<br>$\frac{B'A'}{BA} = \frac{B'P}{BP}$   |                |   |
| : Linear magnification<br>$\frac{B'P}{BP} = \frac{+v}{-u} = -\frac{v}{u}$  | 1/2            |   |
| 18 Obtaining Expression for the equivalent   |                |   |
| (i)resistance1(ii)emf2   |                |   |
| $\begin{array}{c} \overbrace{I_1} \\ \overbrace{I_2} \\ \overbrace{I_2} \\ \hline \\ $ | Y <sub>2</sub> |   |
| $\frac{1}{r} = \frac{1}{r_1} + \frac{1}{r_2}$ $\therefore r = \frac{r_1 r_2}{r_1 + r_2}$   | Y <sub>2</sub> |   |
| $I = I_1 + I_2$ $V = E_1 - I_1 r_1  and  V = E_2 - I_2 r_2$ $\therefore I = \left(\frac{E_1 - V}{r_1}\right) + \left(\frac{E_2 - V}{r_2}\right)$                       | ¥₂             |   |
| $V = \left(\frac{E_1 r_2 + E_2 r_2}{r_1 + r_2}\right) - I\left(\frac{r_1 r_2}{r_1 + r_2}\right)$   | 1/2            |   |
| also $V = E_{eq} - Ir_{eq}$  | 1/2            |   |
| $\Longrightarrow \frac{E_{eq}}{r_{eq}} = \frac{E_1}{r_1} + \frac{E_2}{r_2}$  | 1/2            |   |
|  |                |   |
| 19   |                | 3 |
| <ul> <li>(a) Two points of difference ½ + ½ Mark</li> <li>(b) Formula ½ Marks</li> <li>Calculation of wavelength 1½ Mark</li> </ul>                                    |                |   |
|  |                |   |

| Any two point of difference :<br>Interference  | Diffraction  |                   |   |
|--|--|-------------------|---|
| Fringes are equally spaced.  | Fringes are not equally spaced.  |                   |   |
| Intensity is same for all maxima   | Intensity falls as we go to successive                                   |                   |   |
|  | maxima away from the centre.   |                   |   |
| Superposition of two waves   | Superposition of a continuous family                                     |                   |   |
| originating from two narrow slits.   | of waves originating from each point on a single slit.                   | $y'_{2} + y'_{2}$ |   |
| Maxima along an angle $\lambda$ /a for two   | Minima at an angle of $\lambda/a$ for a                                  |                   |   |
| narrow slits separated by a  | single slit of width a.  |                   |   |
| distance a.  |  |                   |   |
| (b)<br>Let D be the distnce of the screen from<br>We have                              | n the plane of the slits.  |                   |   |
| Fring width $\beta = \frac{\lambda D}{d}$<br>In the first case                         |  | 1/2               |   |
| $\beta = \frac{\lambda D}{d}$ or $\beta d = \lambda D$                                 | (i)  |                   |   |
| $p = \frac{1}{d}$ or $pd = \pi D$  |  | 1/2               |   |
| $(\beta - 30 \times 10^{-6}) = \frac{\lambda(D - 0.05)}{d}$ or $(\beta - 30)$          | $\times 10^{-6}$ )d = $\lambda$ (D - 0.05)                               | 1/2               |   |
| Subtracting (ii) from (i) we get<br>$30 \times 10^{-6} \times d = \lambda \times 0.05$ |  |                   |   |
| :. $\lambda = \frac{30 \times 10^{-6} \times 10^{-3}}{5 \times 10^{-2}} \text{ m}$     |  |                   | 3 |
|  |  | 1/2               |   |
| $\therefore \lambda = 6 \times 10^{-7} \mathrm{m} = 600 \mathrm{nm}$                   |  | ,,,               |   |
| a) Intensity of linearly polarized<br>Dependence on orientation<br>Explanation         | - ½<br>- 1   |                   |   |
| b) Graphical representation  | - 1  |                   |   |
| a) The intensity of the linearly po<br>No; it does not depend on the                   |  | 1/2<br>1/2        |   |
| Explanation : The polaroid will let the to its pass axis, to pass through it irres     | component of the unpolarized light, parallel pective of its orientation. | 1                 |   |
| b) We have $I = I_0 cos^2 \theta$<br>∴ The graph is as shown below                     | v  |                   |   |
|  |  |                   |   |

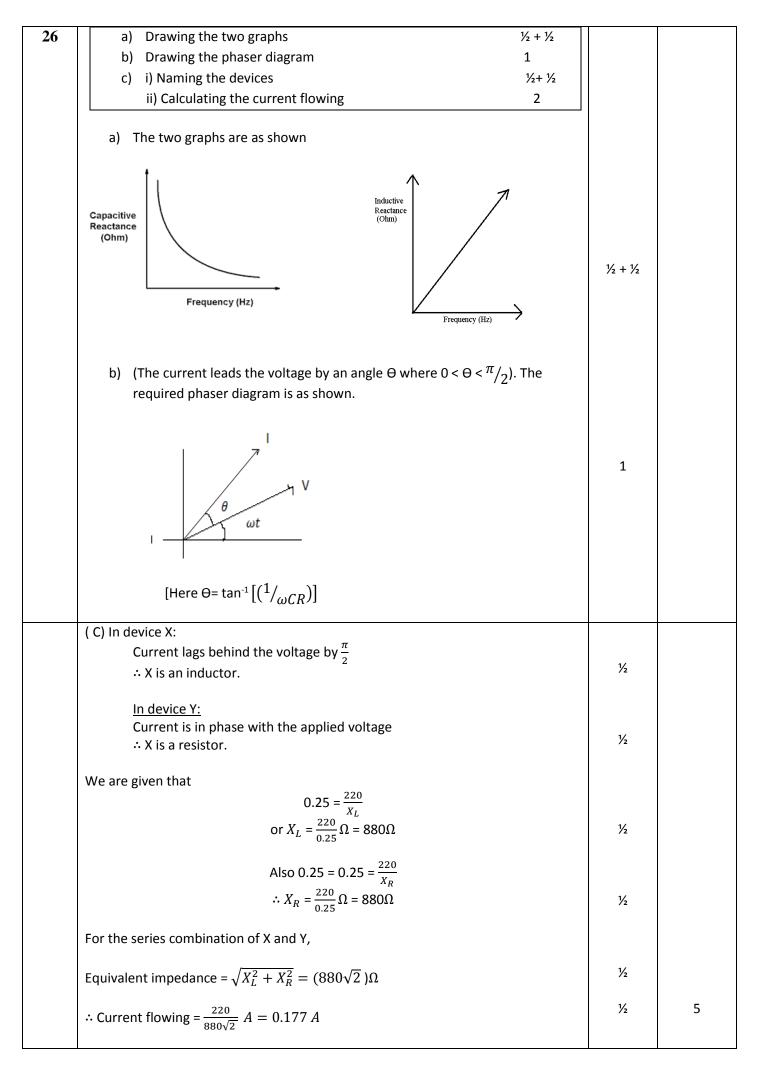
|    |  |                                      | $1$ $1$ $10/2$ $\frac{\pi}{2}$        |                                    | $\frac{3\pi}{2}$ $2\pi$                | ∕x   | 1        | 3 |
|----|--|--------------------------------------|---------------------------------------|------------------------------------|--|--|----------|---|
| 21 | <ul> <li>a) Writing the truth table -1</li> <li>b) Photodiode and its operation - 1 + 1</li> <li>(a) The inputs of the third gate are A and B. Hence the truth table is as given below.</li> </ul>   |                                      |                                       |                                    |  |  |          |   |
|    | A     B $\overline{A}$ $\overline{B}$ C       0     0     1     1     0  |                                      |                                       |                                    |  |  |          |   |
|    | 0  | 1<br>0                               | 1<br>0                                | 0                                  | 0                                      |  | 1        |   |
|    | 1  | 1                                    | 0                                     | 0                                  | 1                                      | for $\overline{A}$ and $\overline{B}$ in her/ his answer)                          |          |   |
|    | (b) A<br>transp<br>Incident I  | photodioo<br>arent wir<br>ight, with | de is a spe<br>ndow to al<br>n photon | ecial purp<br>llow light<br>energy | oose $p -$<br>to fall on<br>greater th | $m{n}$ junction diode fabricated with a the diode. The the energy gap of the semi- | ½<br>1∕2 |   |
|    | conductor, generates electron -hole pairs. The magnitude of the photo current<br>depends on the intensity of intensity of incident light.<br>The photodiode is usually operated under reverse bias conditions.<br>This is because this makes it easier to detect changes in light intensity and makes  |                                      |                                       |                                    |  | 1/2  | 3        |   |
| 22 | This is because this makes it easier to detect changes in light intensity and makes the photodiode work as a detector of optical signals.         Statement of equation with explanation of symbols – 1         Expression for         i. Planck's constant       -1         ii. Work function       -1         Einstein's photoelectric equation is |                                      |                                       |                                    |  | <i>Y</i> <sub>2</sub>  |          |   |
|    | $hv = hv_0$ $v = freque$ $v_0 = thre$ $W = wor$  | uency of<br>shold fr                 | incident<br>equency                   | light                              | ) sensitiv                             | e material   | 1/2      |   |
|    | 1  |                                      |                                       | nergy of                           | <sup>f</sup> the emi                   | tted photoelectrons  | 1∕2      |   |
|    | (Also acce   | pt if the s                          | tudent wr                             |                                    | = W + el                               | /s   |          |   |
|    |  | N                                    | W = work                              |                                    | of photose<br>pping Pote               | ensitive material<br>ntial)  |          |   |
|    | From Eins  | tein's pho                           | otoelectric                           | equatior                           | n, we have                             |  |          |   |

|    | $hv = W + \frac{1}{2} m v_{max}^2$  |            |   |
|----|---|------------|---|
|    | $\therefore v_{max}^2 = \frac{2}{m} (hv - W)$   |            |   |
|    | $=\left(\frac{2h}{m}\right)\nu+\left(\frac{-2W}{m}\right)$  |            |   |
|    | Slope of the given graph = $\frac{l}{n}$<br>Intercept on the y – axis = $-l$  | 1∕2<br>1∕2 |   |
|    | $\therefore \frac{2h}{m} = \frac{\ell}{n} \text{ or } \hbar = \frac{m\ell}{2n}$   | 1∕2        |   |
|    | and - $\ell = \frac{-2W}{m}$ or $W = \frac{m\ell}{2}$   | 1/2        | 3 |
|    | SECTION D   |            |   |
| 23 |   |            |   |
|    | <ul> <li>(a) Name of e.m. radiation ½ Mark</li> <li>(b) Method of production ½ Mark</li> <li>(c) Range of wavelength 1 Mark</li> <li>(d) Two values 1 + 1 Marks</li> </ul>  |            |   |
|    | (a)   | 1∕₂        |   |
|    | (b)<br>(Alternatively : By bombarding a metal target with high energy electrons)  | 1/2        |   |
|    | (c) Wave length range of X-rays is from about (10 nm to 10 <sup>-4</sup> nm)  | 1          |   |
|    | (d) Alertness, empathy; concern for her mother, knowledgeable (any two)   | (1 + 1)    | 4 |
|    | Section E   |            |   |
| 24 | <ul> <li>a) Explaining the two processes-<br/>Defining the two terms -<br/>b) Circuit diagram<br/>Working<br/>-1</li> </ul>   |            |   |
|    | a) The two important processes are diffusion and drift  | 1/2        |   |
|    | Due to concentration gradient, the electrons diffuse from the $n$ side to the   |            |   |
|    | p side and holes diffuse from the $\rho$ side to the $n$ side.  | 1/2        |   |
|    | p side and holes diffuse from the $\rho$ side to the $n$ side.<br>Electron drift $\stackrel{\longleftarrow}{\longrightarrow}$ Electron diffusion<br>p $\stackrel{\bigcirc \ominus \oplus \oplus}{\ominus \ominus \oplus \oplus}$ n<br>$\stackrel{\ominus \ominus \oplus \oplus}{\ominus \ominus \oplus \oplus}$ n | ¥₂<br>¥₂   |   |
|    | p side and holes diffuse from the $\rho$ side to the $n$ side.<br>Electron drift $\stackrel{\longleftarrow}{\longrightarrow}$ Electron diffusion<br>$p \stackrel{\Theta \oplus \Theta \oplus}{\Theta \oplus \Theta \oplus} n$<br>$p \stackrel{\Theta \oplus \Theta \oplus}{\Theta \oplus \Theta \oplus} n$        |            |   |

| Depletion region:   |                          |   |
|---|--------------------------|---|
| It is the space charge region on either side of the junction, that gets depleted of free  | 1/2                      |   |
| charges, is known as the depletion region.  | , _                      |   |
|   |                          |   |
| Potential Barrier   |                          |   |
|   |                          |   |
| The potential difference, that gets developed across the junction and opposes the   | 1/2                      |   |
| diffusion of charge carries and brings about a condition of equilibrium, is known as  |                          |   |
| the barrier potential.  |                          |   |
|   |                          |   |
| b) The circuit diagram is as shown  |                          |   |
|   |                          |   |
|   |                          |   |
| Voltmeter(V)  |                          |   |
|   |                          |   |
|   |                          |   |
|   | 1                        |   |
| p n   |                          |   |
|   |                          |   |
| Milliammeter<br>(mA)  |                          |   |
|   |                          |   |
| Switch  |                          |   |
| ´+' '- (a)  |                          |   |
| (m)   |                          |   |
| Working   |                          |   |
| -   |                          |   |
| In forward bias condition, the direction of the applied voltage is opposite to the  |                          |   |
| barrier potential. This reduces the width of the depletion layer as well as the height  |                          |   |
| of the barrier. A current can, therefore, flow through the circuit. This current  | 1                        |   |
| increases ( non linearly) with increase in the applied voltage.   | 1                        | - |
|   |                          | 5 |
|   |                          |   |
| OR  |                          |   |
|   |                          |   |
|   |                          |   |
| a) Describing the three factors – 3   |                          |   |
|   |                          |   |
|   |                          |   |
| b) Drawing the wave forms – 2   |                          |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the</li> </ul>  |                          |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:</li> </ul>   | 1/                       |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ul> <li>i. Size of the antenna or aerial</li> </ul> </li> </ul>   | <u>½</u>                 |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li><u>Size of the antenna or aerial</u><br/>This size needs to be comparable to the wavelength of the signal.</li> </ol> </li> </ul>   | 1/2<br>1/2               |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> </ol> </li> </ul>   | 1∕₂                      |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li><u>Size of the antenna or aerial</u><br/>This size needs to be comparable to the wavelength of the signal.</li> </ol> </li> </ul>   |                          |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> </ol> </li> </ul>  | 1∕₂                      |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated<br/>Power radiated, being proportional to (ℓ/λ)<sup>2</sup> would be very small for</li> </ol> </li> </ul>  | 1∕2<br>1∕2               |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated<br/>Power radiated, being proportional to (ℓ/λ)<sup>2</sup> would be very small for<br/>a audio frequency signal.</li> </ol> </li> </ul>  | 1∕2<br>1∕2               |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated<br/>Power radiated, being proportional to (ℓ/λ)<sup>2</sup> would be very small for</li> </ol> </li> </ul>  | ½<br>½<br>½              |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated<br/>Power radiated, being proportional to (ℓ/λ)<sup>2</sup> would be very small for<br/>a audio frequency signal.</li> </ol> </li> </ul>  | 1∕2<br>1∕2               |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons:         <ol> <li>Size of the antenna or aerial<br/>This size needs to be comparable to the wavelength of the signal.<br/>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated<br/>Power radiated, being proportional to (ℓ/λ)<sup>2</sup> would be very small for<br/>a audio frequency signal.</li> <li>Mixing up of different signals</li> </ol> </li> </ul>  | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing</li> </ol> </li> </ul>  | ½<br>½<br>½              |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal.</li> <li>It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if</li> </ol> </li> </ul>  | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (<sup>ℓ</sup>/<sub>λ</sub>)<sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> </ul>  | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing</li> </ol> </li> </ul>  | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (<sup>ℓ</sup>/<sub>3</sub>)<sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown</li> </ul>   | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals.</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> </ol> </li> </ul>                               | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms – 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals.</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> </ol> </li> </ul>                               | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |
| <ul> <li>b) Drawing the wave forms - 2</li> <li>a) It is necessary to modulate the audio frequency signals because of the following three reasons: <ol> <li>Size of the antenna or aerial</li> <li>This size needs to be comparable to the wavelength of the signal. It would be unmanageably long for audio frequency signals.</li> <li>ii. Effective power readiated</li> <li>Power radiated, being proportional to (ℓ/λ) <sup>2</sup> would be very small for a audio frequency signal.</li> <li>Mixing up of different signals</li> <li>The audible frequency range is quite small. Hence if transformisson is done at audio frequencies, the chances of mixing up of different signals are very high.</li> </ol> </li> <li>b) The required wave forms are as shown <ol> <li>Carrier wave</li> <li>Modulating Signal</li> </ol> </li> </ul> | 1/2<br>1/2<br>1/2<br>1/2 |   |



| Give full credit of part (ii) if a student writes that the point (x,y,0) is equidistant   |     |  |
|---|-----|--|
| from charges +q and -q, Hence total potential due to them at the given point will   |     |  |
| be zero.  |     |  |
| (b) Work done = q $[V_1 - V_2]$   |     |  |
| $V_1 = 0$ and $V_2 = 0$   | 1/2 |  |
| $\therefore$ work done = 0  | 1/2 |  |
| Where $V_1$ and $V_2$ are the total potential due to dipole at point (5,0,0) and (-7,0,0)   |     |  |
| (c) There would be no change  | 1/2 |  |
| This is because the electrostatic field is a conservative field.  | 1/2 |  |
| ( <b>Alternatively :</b> The work done, in moving a test charge between two given points is independent of the path taken)  |     |  |
| (d) The two given charges make an electric dipole of dipole moment $\vec{p} = q. \overrightarrow{2a}$   |     |  |
| P.E. in position of unstable equilibrium (where $\vec{p}$ and $\vec{E}$ are antiparallel to each  | 1/2 |  |
| other)  |     |  |
| = + pE = 2 aq E   | 1/2 |  |
| OR  | 72  |  |
|   |     |  |
| <ul> <li>(a) Finding the total energy before the capacitors are connected 1 Mark</li> <li>(b) Finding the total energy in the parallel combination 3 Marks</li> <li>(c) Reason for difference 1 Mark</li> </ul> |     |  |
| (a) We have   |     |  |
| Energy Stored in a capacitor = $\frac{1}{2}CV^2$  |     |  |
| 2   | 1/2 |  |
| : Energy stored in the charged capacitors $E_1 = \frac{1}{2}C_1V_1^2$ And $E_2 = \frac{1}{2}C_2V_2^2$   |     |  |
| $\therefore$ Total energy stored = $\frac{1}{2}C_1V_1^2 + C_2V_2^2$   | 1/2 |  |
| (b)Let V be the potential difference across the parallel combination.   |     |  |
| Equivalent capacitance = $(C_1 + C_2)$  | 1/2 |  |
|   |     |  |
| Since charge is a conserved quantity, we have   |     |  |
| $(C_1 + C_2)V = C_1V_1 + C_2V_2$  | 1/2 |  |
| $V = \left[\frac{C_1V_1 + C_2V_2}{(C_1 + C_2)}\right]$  | 1   |  |
| $\begin{bmatrix} (C_1 + C_2) \end{bmatrix}$   |     |  |
| .:<br>Total energy stored in the parallel combination   |     |  |
|   |     |  |
| $= \frac{1}{2}(C_1 + C_2)V^2$   | 1/2 |  |
| $1(C_1V_1 + C_2V_2)^2$  |     |  |
| $= \frac{1}{2} \frac{(C_1 V_1 + C_2 V_2)^2}{(C_1 + C_2)}$   | 1/  |  |
| (c) The total energy of the parallel combination is different (less) from the   | 1/2 |  |
| total energy before the capacitors are connected. This is because some  |     |  |
|   |     |  |
|   | 1   |  |
| energy gets used up due to the movement of charges during sharing of charge.  | 1   |  |



|                               | OR   |                                 |   |
|-------------------------------|--|---------------------------------|---|
| a) Pri                        | incipal of working – 1   |                                 |   |
| b) De                         | efining efficiency – 1   |                                 |   |
| c) An                         | ny two factor – $\frac{1}{2}$ + $\frac{1}{2}$  |                                 |   |
| d) Ca                         | alculating the current drawn - 2   |                                 |   |
| (Alt<br>flux                  | ransformer works on the principle of mutual induction.<br>ternatively – an emf is induced in the secondary coil when the magnetic<br>, linked with it changes with time due to ta (time) changing magnetic<br>, linked with the primary coil). | 1                               |   |
| inpu<br>( <i>Alt</i><br>Effic | e efficiency of a transformer equals the ratio of the output power to the<br>ut power.<br><i>Iteratively</i> :<br>ciency = $\frac{output power}{input power}$  |                                 |   |
| or E                          | Efficiency $\frac{V_S I_S}{V_P I_P}$   | 1                               |   |
| ii) jo<br>iii) h<br>iv) n     | ddy current losses<br>oule heat losses<br>hysteresis losses<br>magnetic flux leakage losses<br>ny two)   | Y <sub>2</sub> + Y <sub>2</sub> |   |
| (d) We                        |  | 1∕₂                             |   |
| $\therefore \frac{22}{22}$    | $\frac{20}{12}\frac{I_s}{I_p} = 0.9$   |                                 |   |
| or -                          | $\frac{I_s}{I_p} = \frac{0.9}{0.1} = 9$  | ⅓                               |   |
|                               | $p = \frac{I_s}{9} = \frac{(22/_{440})}{9} A$  | 1∕2                             |   |
| $=\frac{1}{18}$               | 1 <sub>30</sub> A  |                                 | 5 |
| = 0.0                         | .0056A   | 1∕₂                             |   |